

$V_{o1} = \text{output 1}$
(left op amp)

P1

KCL's: $-\frac{V_{in}}{R_1} - \alpha V_x - \frac{V_{o1}}{R_2} = 0$ (1)

ideal op amps:

$$V_{n1} = V_{p1} = 0$$

$$\frac{V_{o1} - V_{out}}{R_4} + \frac{V_{o1}}{R_3} = 0$$
 (2)

$$V_{o1} = V_{p2} = V_{n2}$$

(no current through R_5)

$$(2) \rightarrow V_{o1} = V_{out} \frac{1}{R_4} \left(\frac{1}{1/R_4 + 1/R_3} \right)$$

$$V_x = V_{out} - V_{o1}$$

$$(2) \rightarrow (1): 0 = -\frac{V_{in}}{R_1} - \alpha V_{out} + V_{o1} \left(\alpha - \frac{1}{R_2} \right)$$

$$0 = -\frac{V_{in}}{R_1} - \alpha V_{out} + \frac{V_{out}}{R_4} \frac{1}{1/R_4 + 1/R_3} \left(\alpha - \frac{1}{R_2} \right)$$

$$\rightarrow \frac{V_{out}}{V_{in}} = \frac{1}{R_1} \left[-\alpha + \frac{1}{1 + R_4/R_3} \left(\alpha - \frac{1}{R_2} \right) \right]^{-1}$$

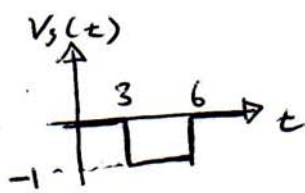
$$\therefore \text{gain} = \frac{1}{R_1} \left[-\alpha + \frac{R_3}{R_3 + R_4} \left(\alpha - \frac{1}{R_2} \right) \right]^{-1}$$

or simplify

$$\text{gain} = -\frac{R_2 (R_3 + R_4)}{R_1 R_3 + \alpha R_1 R_2 R_4}$$

P2

(a)



$-\infty < t < 3$: $V_c(t) = 0$

$3 < t < 6$: $V_c(3) = 0$ $V_c(\infty) = -1$

$$V_c(t) = e^{-(t-3)/R_1 C} - 1$$

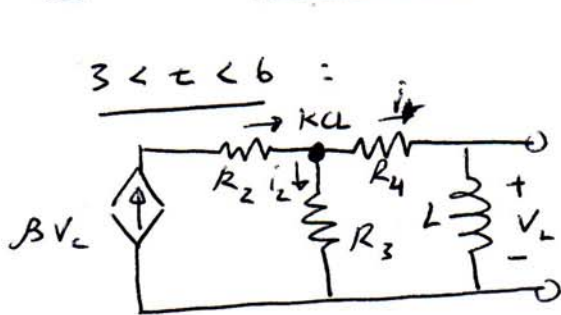
$6 < t$: $V_c(6) = e^{-3/R_1 C} - 1$

$$V_c(t) = V_c(6) e^{-(t-6)/R_1 C} = (e^{-3/R_1 C} - 1) e^{-(t-6)/R_1 C}$$

$$\therefore V_c(t) = \begin{cases} 0 & t < 3 \\ e^{-(t-3)/R_1 C} - 1 & \text{for } 3 < t < 6 \\ (e^{-3/R_1 C} - 1) e^{-(t-6)/R_1 C} & 6 < t \end{cases}$$

(b)

$-\infty < t < 3$: $V_L(t) = 0$ $V_L = L \frac{di_L}{dt}$



$3 < t < 6$:

$$\beta V_c = i_L + i_2 = i_L + \frac{(i_L R_4 + L \frac{di_L}{dt})}{R_3}$$

$$= i_L \left(\frac{R_3 + R_4}{R_3} \right) + \frac{L}{R_3} \frac{di_L}{dt}$$

$$\rightarrow i_L \left(\frac{R_3 + R_4}{L} \right) + \frac{di_L}{dt} = \frac{R_3}{L} \beta V_c$$

for $3 < t < 6$,

$$\therefore \underbrace{i_L \left(\frac{R_3 + R_4}{L} \right)}_k + \frac{di_L}{dt} = \underbrace{\frac{R_3}{L} \beta}_{kA} \left[e^{-(t-3)/R_1 C} - 1 \right]$$

$$\rightarrow i_L = \frac{R_3 \beta}{R_3 + R_4 - \frac{L}{R_1 C}} \left[e^{-(t-3)/R_1 C} - 1 \right]$$

$$V_L = L \frac{di_L}{dt} = \frac{R_3 L \beta}{R_3 + R_4 - L/R_1 C} \left(-\frac{1}{R_1 C}\right) e^{-(t-3)/R_1 C}$$

$$V_L(t) = \frac{-R_3 L \beta}{R_1 C (R_3 + R_4) - L} e^{-(t-3)/R_1 C}$$

6 < t :

$$i_L \left(\frac{R_3 + R_4}{L} \right) + \frac{di_L}{dt} = \frac{R_3}{L} \beta \underbrace{(e^{-3/R_1 C} - 1)}_{kA} e^{-\underbrace{(t-6)/R_1 C}_m}$$

$$\rightarrow i_L = \frac{R_3 \beta (e^{-3/R_1 C} - 1)}{R_3 + R_4 - L/R_1 C} e^{-(t-6)/R_1 C}$$

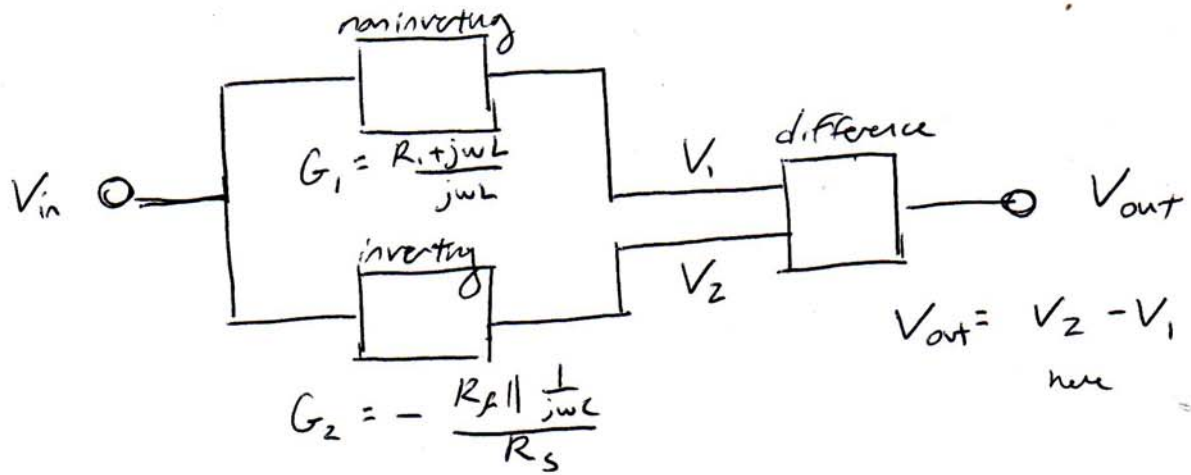
$$V_L(t) = \frac{L R_3 \beta (e^{-3/R_1 C} - 1)}{R_3 + R_4 - L/R_1 C} \left(-\frac{1}{R_1 C}\right) e^{-(t-6)/R_1 C}$$

$$= - \frac{L R_3 \beta (e^{-3/R_1 C} - 1)}{R_1 C (R_3 + R_4) - L} e^{-(t-6)/R_1 C}$$

$$V_L(t) = \begin{cases} 0 & t < 3 \\ -\frac{R_3 L \beta}{R_1 C (R_3 + R_4) - L} e^{-(t-3)/R_1 C} & 3 < t < 6 \\ -\frac{R_3 L \beta (e^{-3/R_1 C} - 1)}{R_1 C (R_3 + R_4) - L} e^{-(t-6)/R_1 C} & 6 < t \end{cases}$$

P3

Interpret as a network of transfer functions:



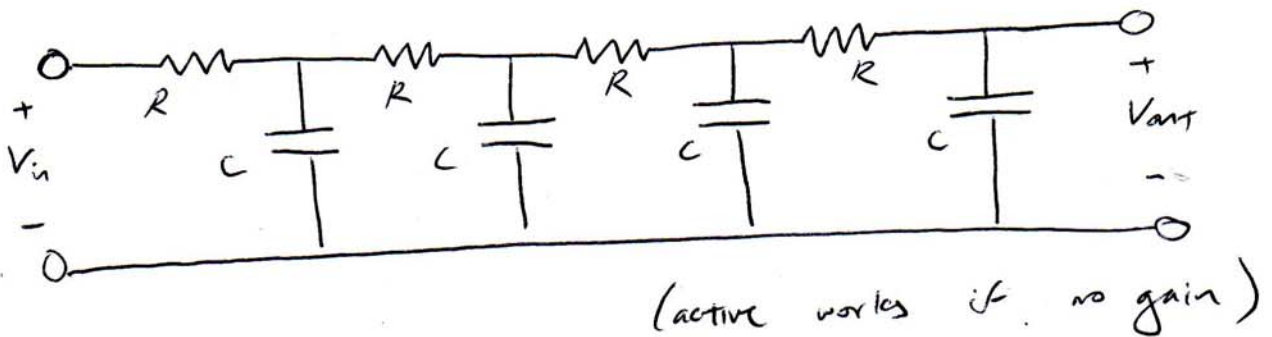
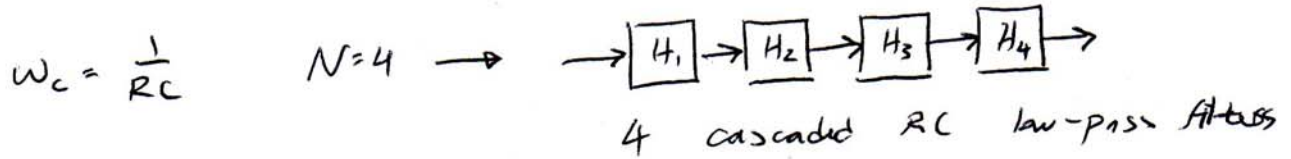
$$\therefore V_{out} = V_2 - V_1 = \left(-\frac{R_f}{R_s} \frac{1}{(1 + j\omega R_f C_f)} - \frac{R_1 + j\omega L}{j\omega L} \right) V_{in}$$

$$H(\omega) = \frac{V_{out}}{V_{in}} = -\frac{R_f}{R_s} \frac{1}{(1 + j\omega R_f C_f)} - \frac{R_1}{j\omega L} - 1$$

P4

4x RC LPF
4x RL LPF
2x LC LPF

(a) multiple implementations exist... here's one:



(b) $|H(\omega)| = \frac{1}{4} \rightarrow$ -12dB

(c) $\phi = 0 - \tan^{-1}(1) = -45^\circ$

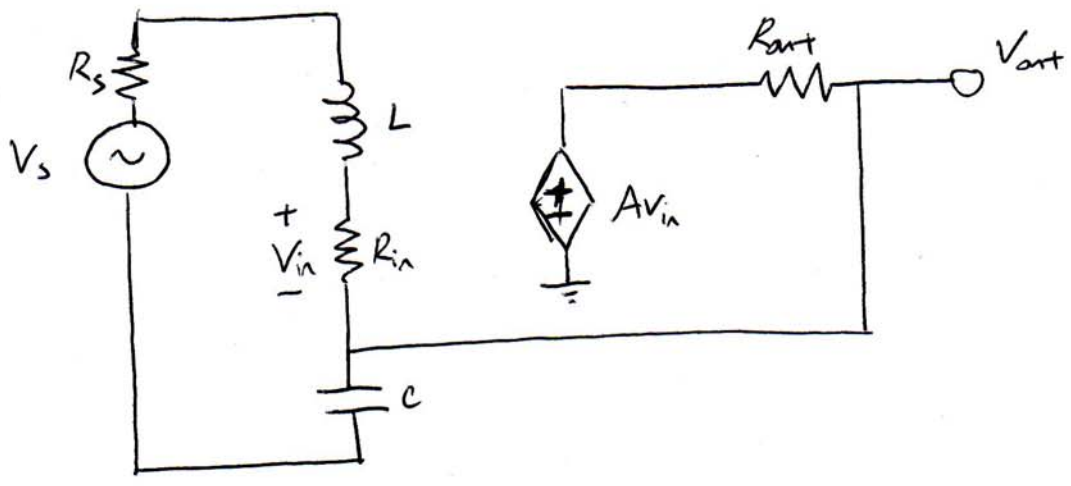
$N=4 \rightarrow$ $\phi = -180^\circ$

or

$\phi = -\pi$

P5

non-ideal



V_{ant} follows phase of $A_{v_{in}}$ since R_{ant} is purely real.

phasor domain:

$$V_{in} = V_s \frac{R_{in}}{R_s + R_{in} + j\omega L + \frac{1}{j\omega C}}$$

no phase shift b/w $V_s \rightarrow V_{in} \rightarrow V_{ant}$
if no imaginary components.

$$\therefore j\omega L + \frac{1}{j\omega C} = 0 \rightarrow \boxed{\omega = \frac{1}{\sqrt{LC}}}$$

$V_s(t)$ is a sinusoidal function with this frequency.

Note: This is the resonance of an RLC circuit!