

$U_1 = 0V$
 $U_2 = 0V$
 $U_{out} = U_1 + U_2 = 0V$ (OR)

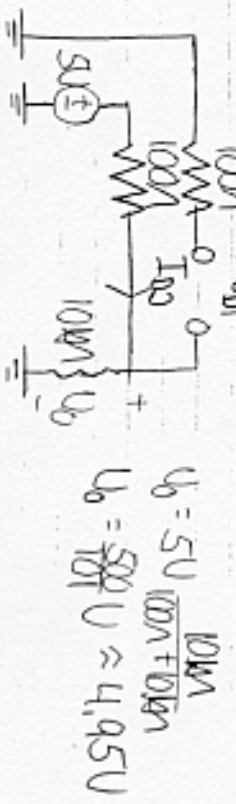
Case 1: $U_1 = 0V$ and $U_2 = 0V$



Assuming that both D1 and D2 are ON and all amperes through I_1 and I_2 are equal to I in the circuit + current amperes same because there is no source in the circuit.
 More that $U_1 = 0V$ for both diodes.
 An OR assumption that the diodes are ON is correct.

①

Case 2: $U_1 = 0V$ and $U_2 = 5V$



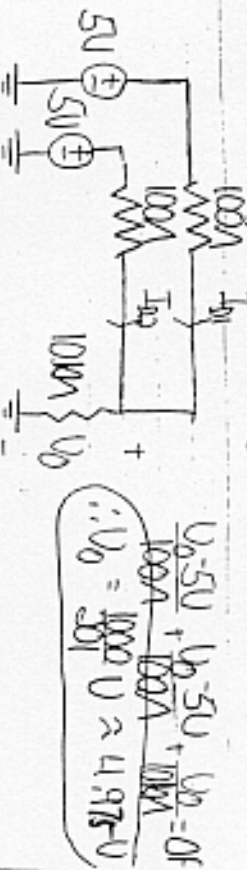
Assuming that D1 is OFF and D2 is ON
 Amperes $U_1 \approx -4.95V$
 Assuming that D1 is OFF and D2 is ON
 Assumption that D2 is ON is correct
 Therefore the average division equation
 answer above applies

Case 3: $U_1 = 5V$ and $U_2 = 0V$

By assumption D1 is ON, D2 is OFF,
 and $U_0 \approx 4.95V$

②

Case 4: $V_1 = 5V$ and $V_2 = 5V$



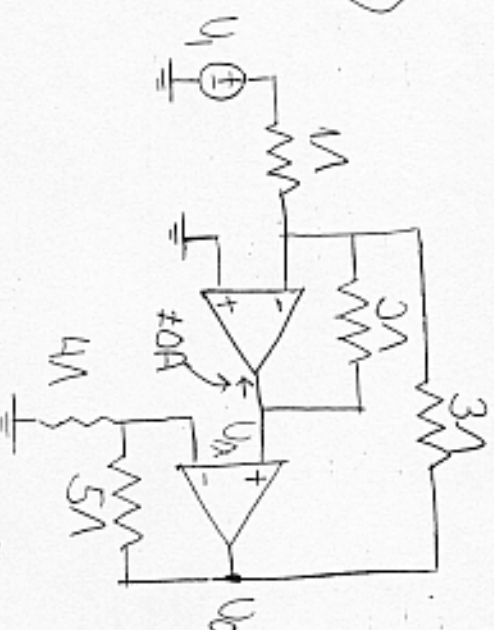
Assume that both I_1 and I_2 are 0A since both I_1 and I_2 are 0A due to KVL application across opamps

$$\frac{V_0 - 5V}{100\Omega} + \frac{V_0 - 5V}{100\Omega} + \frac{V_0 - 0V}{100\Omega} = 0$$

$$\therefore V_0 = \frac{1000}{201} V \approx 4.975V$$

③

2)



$$\frac{A_{v1} - V_1}{1V} + \frac{A_{v1} - V_1}{3V} + \frac{A_{v1} - V_0}{3V} = 0A \quad (\text{KCL at } A_{v1})$$

$$A_{v1} = 0V$$

$$\frac{-V_1}{1V} - \frac{V_0}{3V} - \frac{V_0}{3V} = 0A$$

$$-6V_1 + 3V_0 = 0V$$

$$\frac{A_{v2} - 0V}{4V} + \frac{A_{v2} - V_0}{5V} = 0A \quad (\text{KCL at } A_{v2})$$

$$A_{v2} = V_0$$

$$\frac{V_0}{4V} + \frac{V_0}{5V} - \frac{V_0}{5V} = 0A$$

$$50V_0 + 4V_0 = 4V_0$$

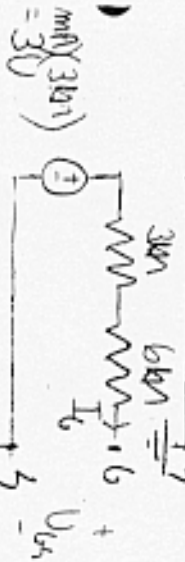
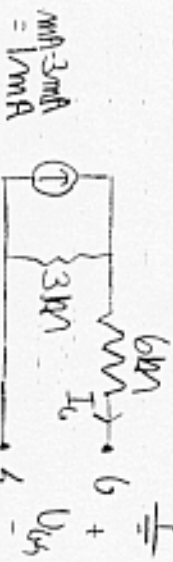
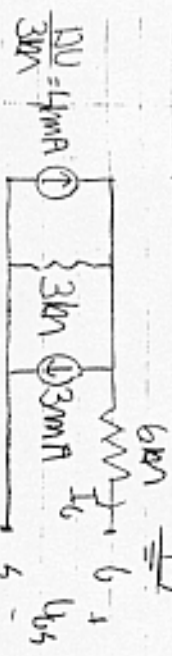
$$V_0 = \frac{4}{9} V_0$$

④

$$6U_1 + 3\left(\frac{4}{3}U_0\right) + 2U_0 = 0U$$

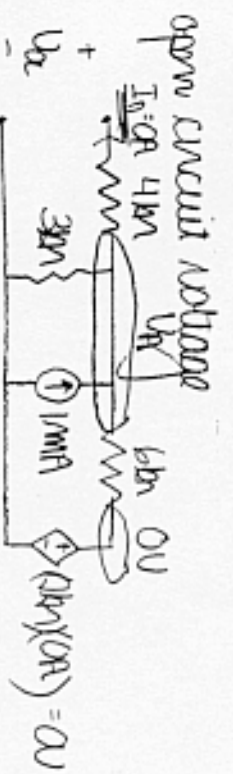
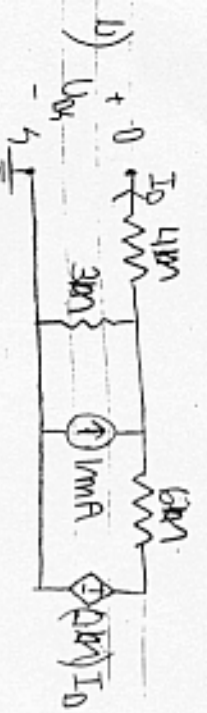
$$6U_1 + \frac{14}{3}U_0 = 0U$$

$$\therefore U_0 = -\frac{18}{14}U_1 = -\frac{9}{7}U_1 = -1.8U_1$$



$$\therefore U_{EN} = 3V$$

$$R_{EN} = 9k\Omega$$



nodal analysis

$$I_a + I_{3k\Omega} + I_{1mA} + I_{6k\Omega} = 0A$$

$$\frac{U_a - 0V}{4k\Omega} - 1mA + \frac{U_a - 0V}{6k\Omega} = 0mA$$

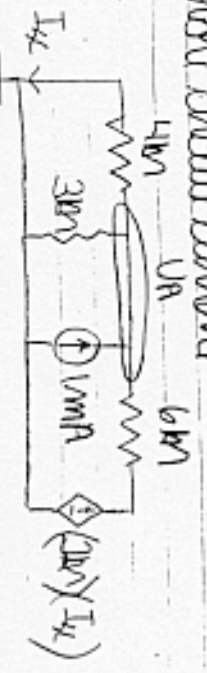
$$U_a = 3V$$

$$\text{Answer } I_0 = 0A$$

$$U_a = U_a = 3V$$

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short circuit current



nodal analysis

$$I_{Ix} + I_{3k\Omega} + I_{1mA} + I_{6k\Omega} = 0A$$

$$\frac{U_a - 0V}{4k\Omega} + \frac{1}{3k\Omega} - 1mA + \frac{U_a - 0V}{6k\Omega} = 0mA$$

$$U_a \left(\frac{1}{4k\Omega} + \frac{1}{3k\Omega} + \frac{1}{6k\Omega} \right) - \frac{1}{3} I_{Ix} = 1mA$$

$$I_{Ix} = \frac{U_a - 0V}{4k\Omega} = \left(\frac{1}{4k\Omega} \right) U_a \Rightarrow \frac{1}{3} I_{Ix} = \frac{1}{6k\Omega} U_a$$

$$U_a \left(\frac{1}{4k\Omega} + \frac{1}{3k\Omega} + \frac{1}{6k\Omega} - \frac{1}{6k\Omega} \right) = 1mA$$

$$U_a = 1.5V$$

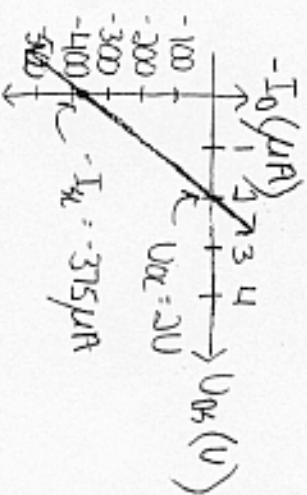
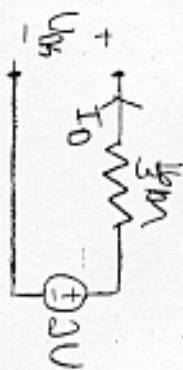
$$I_{Ix} = \frac{U_a - 0V}{4k\Omega} = \frac{1.5V}{4k\Omega} = \frac{3}{8} mA$$

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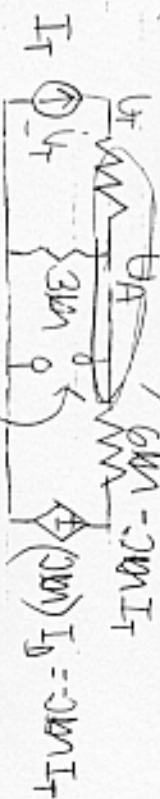
$$V_{in} = V_{ce} = 2V$$

$$I_{D} = I_{ce} = \frac{3}{8} \text{ mA} = 375 \mu\text{A}$$

$$R_{in} = \frac{V_{ce}}{I_{ce}} = \frac{2V}{\frac{3}{8} \text{ mA}} = \frac{16}{3} \text{ k}\Omega = 5.33 \text{ k}\Omega$$



alternative open method to find R_D
(loop source method)



with current source

$$-I_T + \frac{V_A}{3k\Omega} + \frac{V_A + 3V_T I_T}{6k\Omega} = 0A \text{ (KCL at } V_T)$$

$$-6k\Omega I_T + 2V_A + V_A + 3k\Omega I_T = 0V$$

$$3V_A - 4k\Omega I_T = 0V$$

$$V_T - I_T 4k\Omega = V_A$$

$$3(V_T - I_T 4k\Omega) - 4k\Omega I_T = 0V$$

$$3V_T - 16k\Omega I_T = 0V$$

$$\therefore R_{in} = R_{eq} = \frac{V_T}{I_T} = \frac{16}{3} \text{ k}\Omega$$

(6) c)

What is the operating point of the MOSFET M1 (6 pts)? Put your answer in the box below. If you were unable to obtain answers for part a) and/or part b), then use the values shown below. Of course the values may or may not be correct.

part a)

$$V_a = 2V$$

$$R_a = 2k\Omega$$

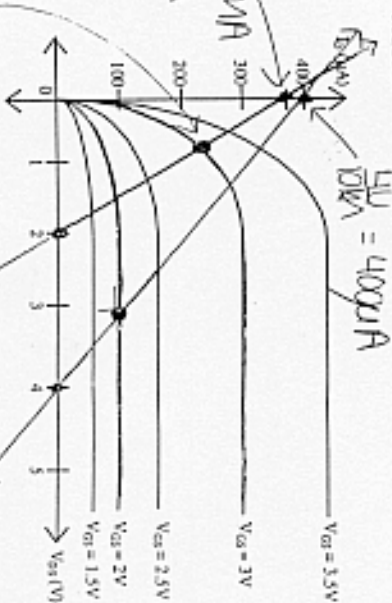
part b)

$$V_a = 4V$$

$$R_a = 10k\Omega$$

Note: We will NOT cascade your errors or take off points for using the above values.

MOSFET M1 IV Curve



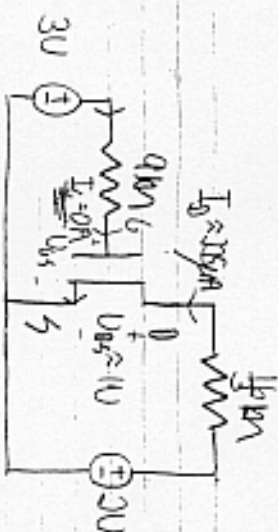
load line using correct values

load line from given values

$$V_{GS} = 0.9V \quad I_D = 325 \mu\text{A}$$

If given values used
 $V_{GS} = 3.11V, I_D = 100 \mu\text{A}$

d)



correct values

$$I_D = 20 \mu\text{A} \quad \sum P_{\text{loss}} = 0 \text{ W}$$

$$P_{\text{out}} + P_{\text{gen}} + P_{\text{gen}} + P_{\text{20V}} + P_{\text{M1}} = 0 \text{ W}$$

$$P_{\text{M1}} = |P_{\text{20V}} - P_{\text{gen}}| \quad (P_{\text{M1}}(\text{correct}) > 0 \text{ W})$$

$$P_{\text{M1}} = |I_D V_{GS} - I_{\text{gen}}^2 R_{\text{gen}}|$$

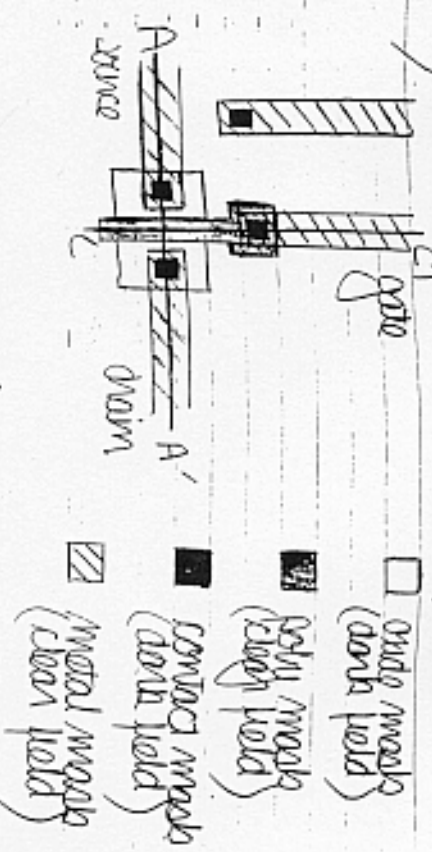
$$P_{\text{M1}} \approx |(205 \mu\text{A})(2V) - (205 \mu\text{A})^2 \left(\frac{10}{3} \text{ k}\Omega\right)|$$

$$\therefore P_{\text{M1}} \approx 180 \mu\text{W}$$

$$P = I_D V_{GS} \approx (205 \mu\text{A})(0.8V) = 180 \mu\text{W}$$

many other possible final answers

4) Process sequence: CMOS transistor



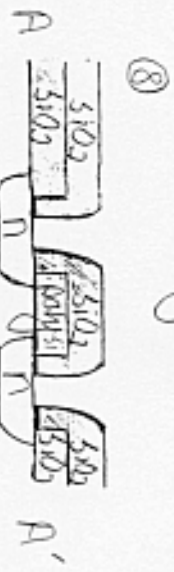
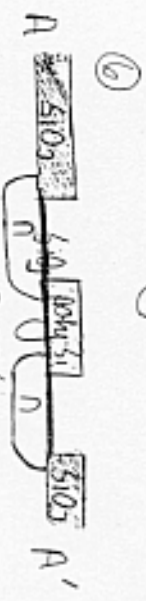
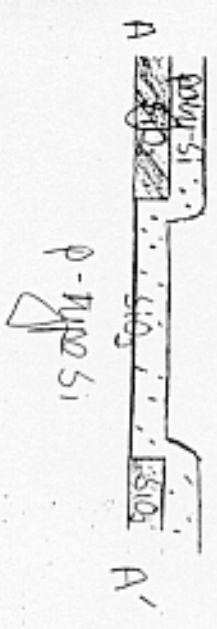
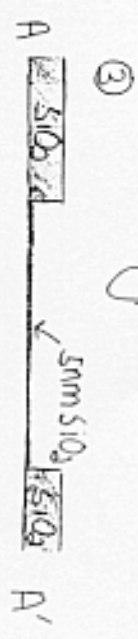
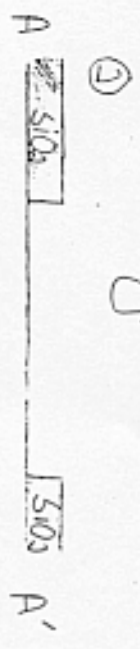
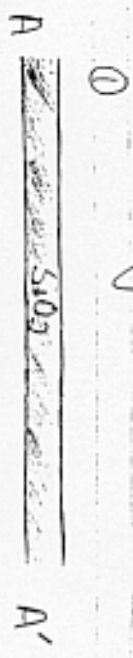
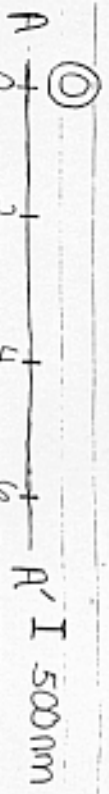
Starting material is a p-type silicon wafer

- ⇒ ① grow 500 nm of SiO₂ (silicon dioxide) (field)
- ② pattern SiO₂ using the oxide mask (dark field)
- ⇒ ③ grow 5 nm of SiO₂ (gate)
- ⇒ ④ deposit 500 nm of n-type polysilicon
- ⑤ pattern polysilicon using the poly mask (clean field)
- ⑥ implant arsenic (10^{19} cm^{-3}) and anneal to form source and drain regions. Note that the arsenic will penetrate the gate oxide but not the polysilicon or field oxide. ⑬

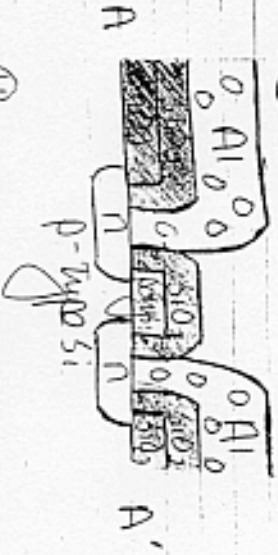
⑦ deposit 500 nm of SiO₂

- ⑧ pattern SiO₂ using contact mask (dark field) and remove polysilicon
- ⑨ deposit 1 μm of Al
- ⑩ pattern Al using metal mask (clean field)
- ⑪ anneal to heal gate oxide damage and make good Si-Al contacts

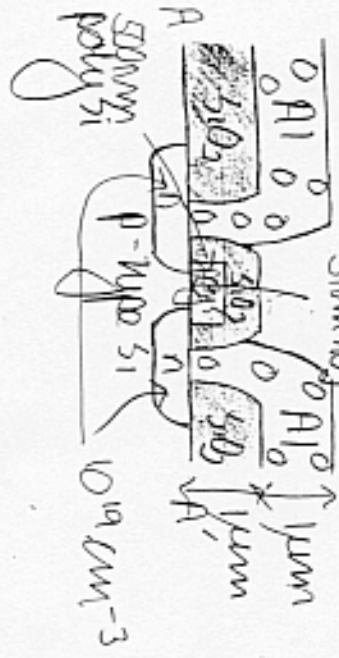
AA' cross-section



⑩



⑪



⑫