1.1

$$V_{0} = (k / f)(V_{1} - V_{2}) \qquad V_{2} = V_{0}R_{1} / (R_{1} + R_{2})$$

$$V_{0} = (k / f)V_{1} - (k / f)V_{0}R_{1} / (R_{1} + R_{2})$$

$$V_{0}[1 + (k / f)R_{1} / (R_{1} + R_{2})] = V_{1}(k / f)$$

$$G = V_{0} / V_{1} = \frac{k / f}{1 + (k / f)R_{1} / (R_{1} + R_{2})} = \frac{1}{(f / k) + R_{1} / (R_{1} + R_{2})} = \frac{R_{1} + R_{2}}{(f / k)(R_{1} + R_{2}) + R_{1}}$$
[10 points off for $G = (R_{1} + R_{2})/R_{1}$]

1.2

$$G = V_0 / V_1 = \frac{1+999}{1+(1+999)(f/10^6)} = \frac{1000}{1+f/10^3} = \frac{10^6}{10^3+f}$$

$$G = 1000 \text{ at } f << 10^2 \text{ Hz} \qquad G = 909 \text{ at } f = 10^2 \text{ Hz} \qquad G = 500 \text{ at } f = 10^3 \text{ Hz}$$

$$G = 90.9 \text{ at } f = 10^4 \text{ Hz} \qquad G = 9.90 \text{ at } f = 10^5 \text{ Hz} \qquad G = 0.999 \text{ at } f = 10^6 \text{ Hz}$$







Infinite open-loop op-amp gain: virtual short rule: $V_+ = V_-$

$$\frac{V_1 - V_-}{R_1} = \frac{V_- - V_0}{R_2} \qquad \frac{V_2 - V_+}{R_1} = \frac{V_+}{R_2}$$

 $V_1R_2 - V_-R_2 = V_-R_1 - V_0R_1$ $V_2R_2 - V_+R_2 = V_+R_1$ Subtracting, $(V_2 - V_1) R_2 = V_0R_1$

$$V_0 = (V_2 - V_1)(R_2/R_1)$$

[7 points off if not in terms of resistors]

2.2 Differential gain
$$V_0 = G_{\pm}(V_2 - V_1) + G_C(V_2 + V_1)/2$$

 $G_{\pm} = R_2/R_1$ Since V₀ does not depend on (V₁ + V₂), G_C = 0

3.1



3.2

The LPF needs to have a gain $G_1 = 0.9$ at $f_1 = 20$ kHz and drop to a gain $G_2 = 0.001$ at $f_2 = 52$ kHz. So we need a filter that has $f_2/f_1 < 2.6$.

n	f_1/f_c	f_2/f_c	ratio	
4	0.834	5.623	6.74	n too low
6	0.886	3.162	3.57	n too low
Oata	hor 6 20	10		

Midterm #1 Solutions – EECS 145L Fall 2010

```
8 0.913 2.371 2.55 n = 8 OK
10 0.930 1.995 2.15 n high, but OK
```

```
\begin{array}{l} (20 \ kHz/0.913) < f_c < (60 \ kHz/2.371) \\ 21.91 \ kHz < f_c < 21.93 \ kHz \end{array}
```

LPF n = 8, $f_c = 21.92 \text{ kHz}$

[3 points off for $f_c = 20$ kHz, which would make the gain 0.707 (too low) at 20 kHz]

[3 points off for n = 12 or 14]

The HPF needs to have a gain $G_1 = 0.9$ at 100 Hz and drop to a gain $G_2 = 0.001$ at 2 Hz. So we need a filter that has $f_1/f_2 < 50$

 $\begin{array}{ll} n & f_1/f_c & f_2/f_c & ratio \\ 2 & 1.437 & 0.032 & 44.9 & n=2 \ OK \\ 4 & 1.199 & 0.178 & 6.74 & n=4 \ high, \ but \ OK \\ (2 \ Hz/0.032) < f_c < (100 \ Hz/1.437) \\ 62.5 \ Hz < f_c < 69.6 \ Hz \\ \end{array}$

HPF n = 2, $f_c = 65 \text{ Hz}$

[3 points off for $f_c = 100$ Hz, which would make the gain 0.707 (too low) at 100 Hz]

This HPF has a gain just a bit below 0.7 at 60 Hz and does not meet the gain requirement of 0.01. A notch filter with accurate components should provide the necessary low gain.

Note: an alternative solution to the notch filter was to use a 10th or 12th order HPF to reduce the gain from 0.9 at 100 Hz to 0.01 at 60 Hz- although this solution uses 2 or 3 more op-amps, costs more, and has more components that can fail, it was accepted.

4.1



[2 points off for not producing an output that varied from 0 to 10 V as the liquid level varied from 0 m to 10 m]

[5 points off for not providing a buffer amplifier between the 10 k Ω sensor resistor and the readout circuit; this is an inferior design where the output voltage is not linearly proportional to liquid level]

4.2 The relationship between liquid height h (in meters) and output voltage V (in volts) is V = h

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October 6, 2010
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Midterm #1 Solutions – EECS 145L Fall 2010

An rms uncertainly of 1 mV in V produces an rms uncertainty in liquid height of 1 mm. [2 points off for mV]

4.3 Determining the change in the liquid level per minute requires making two measurements one minute apart and taking the difference. Making two measurements a and b exactly one minute apart results in a measurement of the change in liquid level f = a - b (in mm per minute).

 $\sigma_a = \sigma_a = 1 \text{ mm} (\text{from part 4.2})$ $\sigma_f^2 = \sigma_a^2 + \sigma_b^2 = 2 \text{ (mm/min)}^2$ $\sigma_f = 1.414 \text{ mm} / \text{min}$ (1.4 mm was accepted for full credit) [2 points off for 1.414 mV/min] [3 points off for 1 mm/min or 2 mm/min] [4 points off for 1 mV/min or 2 mV/min] [5 points off for 0.01%/min] [6 points off for 1 mV or 2 mV]

Note 1: The equation sheet said that if f = k(a - b) then $\sigma_f^2 = k^2(\sigma_a^2 + \sigma_b^2)$ Note 2: The rate of change in liquid level is measured in mm/min, not mV or mV/min.

145L midterm #1 grade distribution:

	8	maximum scor average score =	e = 100 = 85.0 (B) (1	9.2 rms)
Problem				,
1	21.9 (5.1 rms) (25 max)	< 55	3	F
		55-59	0	F
2	22.2 (6.0 rms) (25 max)	60-64	1	D
		65-69	0	D
3	26.7 (7.6 rms) (30 max)	70-74	0	С
		75-79	2	С
4	14.2 (5.6 rms) (20 max)	80-84	1	В
		85-89	3	В
		90-94	5	А
		95-99	3	А
		100	6	A+

EECS average 88.4 (12.1 rms) BioEng average 81.7 (25.8 rms)