

## Midterm #1 Solutions – EECS 145L Fall 2000

**1a**

$$V_0 = (k/f)(V_1 - V_2) \quad V_2 = V_0 R_1 / (R_1 + R_2)$$

$$V_0 = (k/f)V_1 - (k/f)V_0 R_1 / (R_1 + R_2)$$

$$V_0 [1 + (k/f)R_1 / (R_1 + R_2)] = V_1 (k/f)$$

$$G = V_0 / V_1 = \frac{k/f}{1 + (k/f)R_1 / (R_1 + R_2)} = \frac{1}{(f/k) + R_1 / (R_1 + R_2)} = \frac{R_1 + R_2}{(f/k)(R_1 + R_2) + R_1}$$

[10 points off for  $G = (R_1 + R_2)/R_1$ ]

**1b**

$$G = V_0 / V_1 = \frac{100}{1 + f/10^5 \text{ Hz}}$$

$$G = 100 \text{ for } f \ll 10^5 \text{ Hz}$$

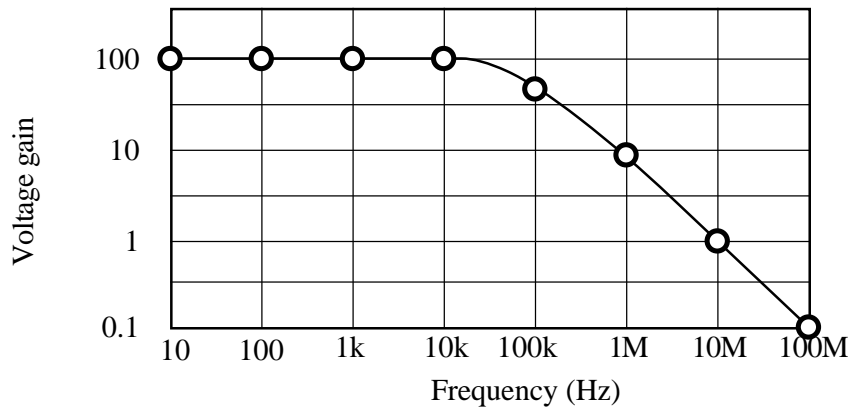
$$G = 91 \text{ for } f = 10^4 \text{ Hz}$$

$$G = 50 \text{ for } f = 10^5 \text{ Hz}$$

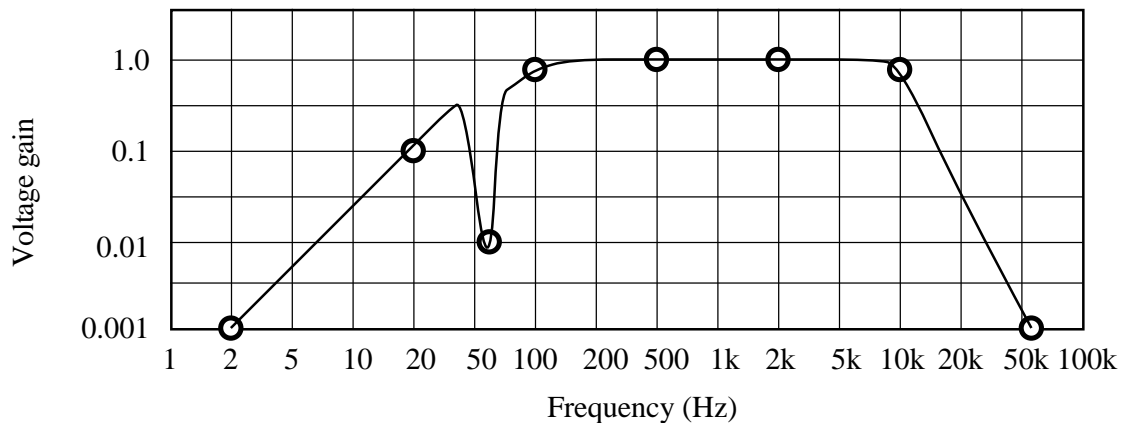
$$G = 9.1 \text{ for } f = 10^6 \text{ Hz}$$

$$G = 1 \text{ for } f = 10^7 \text{ Hz}$$

$$G = 0.1 \text{ for } f = 10^8 \text{ Hz}$$



**2a**



**2b**

The LPF needs to have a gain of 0.9 at 20 kHz and drop to a gain of 0.001 at 52 kHz (frequency ratio 2.6). The Butterworth LPF table shows that an **8th order low pass Butterworth filter** has  $f/f_c = 0.913$  at a gain of 0.9 and  $f/f_c = 2.371$  at a gain of 0.001. This is a frequency ratio of 2.6, as required. A smaller order number has a frequency ratio that is too small and a higher order number would be excessive. The corner frequency  $f_c = 20 \text{ kHz}/0.913 = 21.9 \text{ kHz}$ .

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[ $n = 10$  or  $12$  was also accepted]

The HPF needs to have a gain of 0.9 at 100 Hz and drop to a gain of 0.001 at 2 Hz (frequency ratio 50). The Butterworth HPF table shows that a **second order high pass Butterworth filter** has  $f/f_c = 1.437$  at a gain of 0.9 and  $f/f_c = 0.032$  at a gain of 0.001. This is a frequency ratio of 45, and meets the requirement. A HPF of order 1 would not meet the requirement and a higher order filter would be excessive. The corner frequency  $f_c = 100 \text{ Hz} / 1.437 = 70 \text{ Hz}$ .

[ $n = 4$  was also accepted]

The HPF has a gain just a bit below 0.7 at 60 Hz and does not meet the gain requirement of 0.01. A notch filter with accurate components should provide the necessary low gain.

[3 points off for using a 10 or 12 pole HPF rather than a notch filter to reduce the gain from 0.9 at 100 Hz to 0.01 at 60 Hz- this uses 4 or 5 more op-amps and is inefficient and expensive]

### 3a

To measure common mode gain, connect both inputs of the instrumentation amplifier to a sine wave generator and measure  $V_{in}$  and  $V_{out}$  vs frequency.  $G_c = V_{out}/V_{in}$ .

To measure differential gain, ground one input and connect the other to a sine wave generator and measure  $V_{in}$  and  $V_{out}$  vs frequency. The differential input is  $V_{in}$  and the common mode is  $V_{in}/2$ .

From  $V_{out} = G_{\pm}V_{in} + G_c V_{in}/2$  and  $G_c$  measured above, compute  $G_{\pm}$ .

[4 points off for not providing two inputs]

[1 point off for not correcting for the common mode input  $V_{in}/2$ . Note that the common mode gain couples both the positive and negative inputs equally to the output.]

$$V_0 = G_+V_+ + G_-V_- = G_{\pm}(V_+ - V_-) + G_c(V_+ + V_-)/2$$

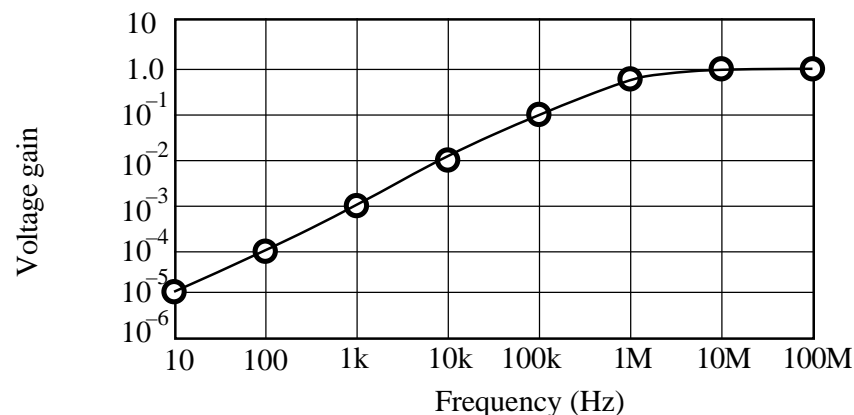
$$G_+ = G_{\pm} + G_c / 2$$

$$\text{If } V_- = 0, \text{ then } V_0 = (G_{\pm} + G_c / 2)V_+$$

An alternative method would be to send  $V_{in}$  through inverting and a noninverting op-amp circuits to generate the pure differential inputs  $V_{in}$  and  $-V_{in}$ .

### 3b

$$G_c = \frac{f / 10^6 \text{ Hz}}{\sqrt{1 + (f / 10^6 \text{ Hz})^2}}$$

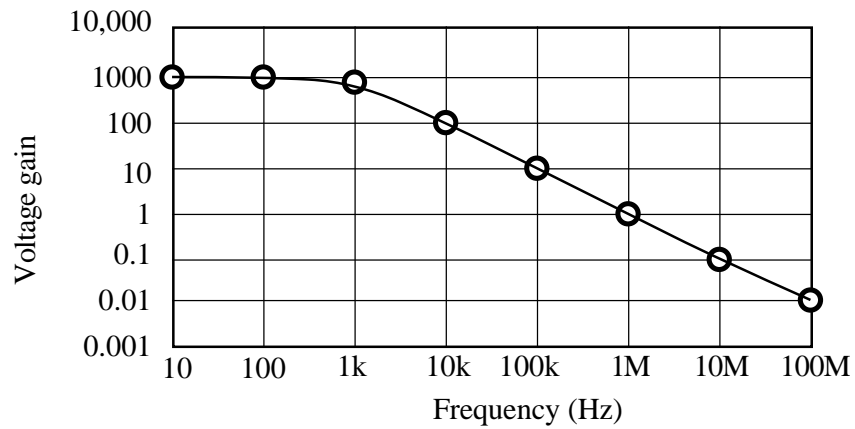


[3 points off for graph but no equation]

# Midterm #1 Solutions – EECS 145L Fall 2000

3c

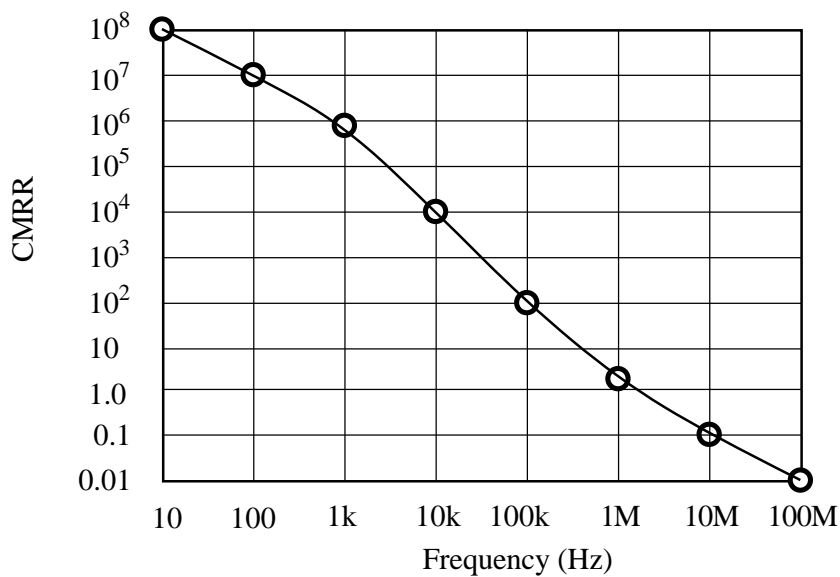
$$G_{\pm} = \frac{1000}{\sqrt{1 + (f / 10^3 \text{Hz})^2}}$$



[3 points off for graph but no equation]

3d

$$\text{CMRR} = G_{\pm} / G_c$$



# Midterm #1 Solutions – EECS 145L Fall 2000

## 145L midterm #1 grade distribution:

Problem

1	25.3 (30 max)
2	31.1 (35 max)
3	25.5 (35 max)

maximum score =	100	
average score =	81.9	
31-40	0	
41-50	2	D
51-60	1	C
61-70	0	
71-80	2	B-
81-90	5	B
91-95	0	
96-100	5	A